

Date: Dec. 4, 2003

Name: EECE 471

Course: M11) TERM 2003

ON MY HONOR, I WILL NOT GIVE OR RECEIVE ANY ASSISTANCE ON THIS QUIZ OR EXAM.

Signature: \_\_\_\_\_

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2.

a)

$$\phi = \cos^{-1} 0.707 = 45^\circ$$

$$Q = P \tan \phi = 500 \text{ kVAR}$$

$$S = 500 + j500 \text{ kVA}$$

$$I = \frac{P - jQ}{\sqrt{3} V_{ll}} = \frac{0.656 - j0.656}{\sqrt{3} \cdot 440} \text{ kA} = 0.928 \angle -45^\circ$$

b)

$$\phi = \cos^{-1} 0.9 = 25.8^\circ$$

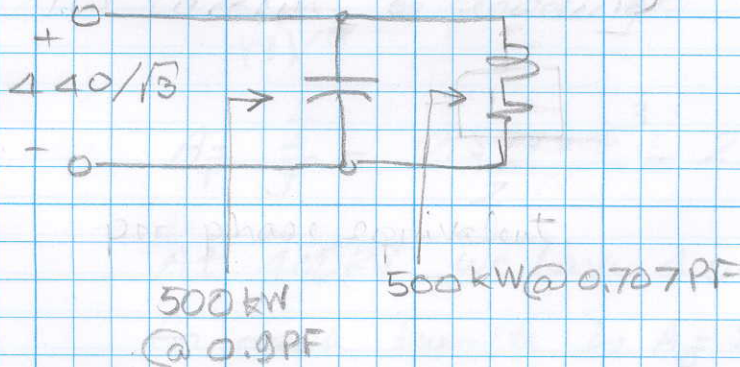
$$Q = P \tan \phi = 500 \times 0.484 = 242 \text{ kVAR}$$

80.6 kVAR / phase.

$$I = \frac{500 - j242}{\sqrt{3} \cdot 440} = 0.656 - j0.318 \text{ kA} = 0.729 \angle -25.8^\circ$$

c)

We need to add a capacitor in parallel with the load in parallel with the line. Where if the main equipment



The reactive power provided by capacitor is:

$$Q_c = 500 - 242 = 258 \text{ kVAR} \quad 86 \text{ kVAR / phase}$$

$$\text{But } Q_c = \frac{(V_{ll})^2}{X_c} \Rightarrow |Y_c| = \frac{Q_c}{(V_{ll})^2} = \frac{258 \times 10^3}{(440)^2} = 1.33 \text{ S}$$

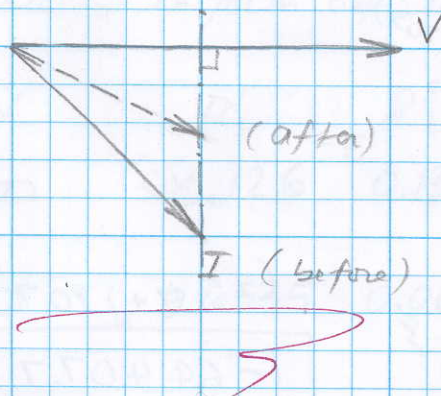
$$|y_c| = \omega C \Rightarrow C = \frac{|y_c|}{2\pi f}$$

$$\text{At } f = 50 \text{ Hz}$$

$$C = \frac{1.33}{2 \times 3.14 \times 50} = 4.23 \text{ mF}$$

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d) Phasor diagram



The compensation improved the overall PF and reduced the magnitude of the current.

3

a)

At 400 kV:

$$I = \frac{P}{\sqrt{3} V_{ll}} = 0.577 \text{ kA}$$

$$A = \frac{I}{J} = \frac{0.577 \times 10^3}{2} = 289 \text{ mm}^2$$

At 400 kV we have 4 bundles, and so the area for each bundle is  $A_b = 289 / 4 = 72.2 \text{ mm}^2 = 142.4 \text{ kmil}^2$

Since this is lower than the smallest in table select smallest: Partridge.

At 220 kV:

$$I = 1050 \text{ A}$$

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$$A_T = \frac{1050}{2} = 525 \text{ mm}^2$$

$$A_c = \frac{525}{2} = 262.5 \text{ mm}^2 = 517.8 \text{ kcmil}$$

Select next higher in the Table: 501e (556.5 kcmil)

b) Put Results in form of Table:

kV	$R_b$ ( $\Omega$ )	$R_b^c$ ( $\Omega$ )	$L$ (mH)	Deq (m)	$r^*$ (m)
400	0.126	0.134	13.5	0.00348 ( $3.48 \times 10^{-3}$ )	
220	0.0535	0.061	9.6	0.01224	

\* radius estimated based on GMR/0.78 or using  $A = \pi r^2$ .

KV	$R$ ( $\Omega$ )	$L$ (mH) $\mu/m$	$C$ ( $\mu F$ ) $F/m$
400	15.4	225 ( $0.935 \times 10^{-6}$ )	2.9 ( $0.12 \times 10^{-10}$ )
220	14.9	250 ( $1.04 \times 10^{-6}$ )	2.6 ( $0.11 \times 10^{-10}$ )

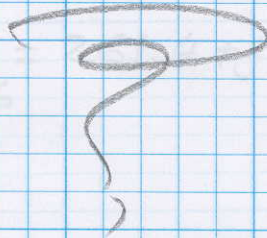
c)

kV	$Z$ ( $\Omega$ )	$Y$ ( $\mu S$ )	$Z_c$ ( $\Omega$ )	$\gamma$ (rad/mile)
400	$15.4 + j70.7$	$j911$	$281 \angle -6.2^\circ$	$0.0017 \angle 84^\circ$
220	$14.9 + j78.5$	$j817$	$313 \angle -5.4^\circ$	$0.0017 \angle 84.5^\circ$

d)

	$P_{SIL}$	$P/P_{SIL}$
400	569.4	0.702
220	154.5	2.59

$P/P_{SIL}$  is above the  $45^\circ$  line on the capability curve and so will be rejected. Select the 400 kV.



4

a) Per Phase Equivalent Load Impedance.

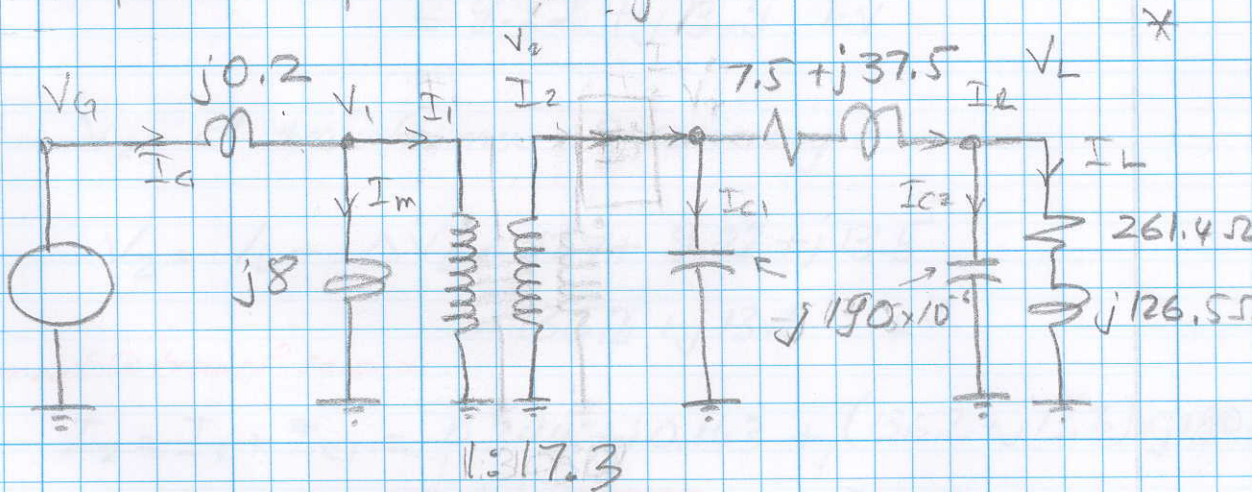
$$Z_L = \frac{V_{ee}^2}{S^*} \quad \text{but } S = P + jQ$$

$$Q = P \tan \phi = 150 \cdot \tan \cos^{-1} 0.9 = 150 + j72.6$$

0.484

$$\therefore Z_L = \frac{220^2}{150 - j72.6} = 261.4 + j126.5 \Omega = 290 \angle 25.8^\circ \Omega$$

b) Per-phase Impedance Diagram



$$Y_c = j3.8 \times 100 \times 10^{-6} = j380 \times 10^{-6} \text{ S} \Rightarrow X_c = -j2.63 \times 10^3 \Omega$$

$$Z_c = (0.075 + j0.375) \times 100 = 7.5 + j37.5 \Omega$$

$$\frac{Y_c}{2} = \frac{j380 \times 10^{-6}}{2} = j190 \times 10^{-6} \text{ S}$$

$$n = \frac{127}{12.7} = 10$$

$$n\sqrt{3} = 17.3$$

\* Disregard  $30^\circ$  phase shift at transformer secondary since this is a normal system.

$$c) V_{en} = 220 / \sqrt{3} = 127 \text{ kV}$$

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Calculate series line current

$$\begin{aligned} I_L = I_L + I_{c2} &= 127 \left[ (261.4 + j126.5) + j190 \times 10^{-6} \right]^{-1} \\ &= 0.394 - j0.191 + j0.024 \\ &= 0.394 - j0.167 \text{ kA} = 0.428 \angle -23^\circ \end{aligned}$$

The voltage drop across line is:

$$\begin{aligned} \Delta V_L = Z_L \times I_L &= (0.394 - j0.167)(7.5 + j37.5) \\ &= 9.22 + j13.5 \text{ kV} \end{aligned}$$

$V_2$  at transformer secondary:

$$\begin{aligned} V_2 = V_L + \Delta V_L &= 127 + 9.22 + j13.5 \\ &= 136.2 + j13.5 \text{ kV} \end{aligned}$$

current @ transf. second:

$$\begin{aligned} I_2 = I_L + I_{c1} &= 0.394 - j0.143 + (136.2 + j13.5) \times j190 \times 10^{-6} \\ &= \boxed{0.391 - j0.117 \text{ kA}} = 0.408 \angle -16.7^\circ \text{ kA} \end{aligned}$$

primary current:

$$I_1 = I_2 \times n\sqrt{3} = \boxed{6.77 - j2.026 \text{ kA}} = 7.067 \angle -16.7^\circ \text{ kA}$$

$$d) V_1 = V_2 / n\sqrt{3} = (136.2 + j13.5) / 17.3 = 7.86 + j0.78 \text{ kV}$$

$$\begin{aligned} I_g = I_1 + I_m &= I_1 + \frac{V_1}{jX_m} = (6.77 - j2.026) + \frac{7.86 + j0.78}{j8} \\ &= 6.8 - j2.03 + 0.098 - j0.98j \\ &= 6.87 - j3.0 \text{ kA} = 7.50 \angle -23.6^\circ \end{aligned}$$

$$\begin{aligned}
 V_G &= V_1 + I_G (jX_D) = (7.86 + j0.78) + (6.87 - j3)(j0.2) \\
 &= 8.46 + j2.15 \text{ kV}
 \end{aligned}$$

$$\begin{aligned}
 P_G + jQ_G &= 3 V_G I_G^* \\
 &= 3 (8.46 + j2.15) (6.87 + j3) = \\
 &= 3 (51.67 + j40.15) \\
 &= 155 + j120.5 \text{ MVA}
 \end{aligned}$$

e)

